



Enhancing longevity and performance: The effects of ZrO₂ and TaC coatings on pistons in internal combustion engines

SATHISH RENGARAJAN¹, RAMEEZA MUHAMMED^{1*}, D. VIJAYAN²
and MUHAMMED ABRAR³

¹Department of Mechanical Engineering, St. Joseph's College of Engineering OMR, Chennai, Tamil Nadu, India, ²Department of Mechanical Engineering, SCSVMV University, Enathur, Kanchipuram, Tamil Nadu, India and ³Department of Mechanical Engineering, St. Joseph's Institute of Technology, OMR, Chennai, Tamil Nadu, India

((Received 24 February, revised 8 April, accepted 21 May 2024)

Abstract: Coating of pistons with ZrO₂ and TaC improves their longevity and performance in internal combustion engines by enhancing the resistance to wear, heat and corrosion. In this study the plasma spray coating is performed on crown of the piston with the combination of the percentage composition namely, 95 % ZrO₂ + 5 % TaC, 98 % ZrO₂ + 2 % TaC and 100 % ZrO₂. Among the three 95 % ZrO₂ + 5 % TaC composition shows better results. The increase in ZrO₂ content leads to the formation of a more integrated scale with fewer pores. Higher concentrations of ZrO₂ in the coatings lead to the increased interaction with discharge sparks and instability of the process. At elevated temperatures, a two-phase material of cubic zirconium dioxide and hexagonal corundum was formed. The bonding strength of the coating is influenced by the addition of TaC and the power input during the spraying operation. The microstructure of ZrO₂ and TaC coatings on aluminium alloy is characterized by granular structure, tightly packed pores and partially melted ZrO₂ particles. The coating had a uniform structure with columnar and cluster-like elements, influenced by ZrO₂ concentration.

Keywords: plasma spray; bond strength; scanning electron microscope; nanoparticles.

INTRODUCTION

The surface characteristics of engineering materials are regarded as crucial in the design process to improve the durability and functionality of components.^{1,2} Wear, corrosion or fatigue mechanisms are the most common causes of damage to engineering parts, which often begins at the surface and occurs during use. The thermal spray coating process is very adaptable and widely recognized

*Corresponding author. E-mail: rama.5.rsj@gmail.com
<https://doi.org/10.2298/JSC240224053R>

as an efficient and cost-effective technique for surface engineering. The most prevalent technique for producing heat barrier coatings in production is plasma spray coatings. Its external high flame temperature makes it an ideal approach for spraying ceramic materials. This technique involves the creation of a coating by propelling small particles that are either melted, semi-molten, or softened towards the surface of the component. When particles strike repeatedly, they mechanically interlock with the surface they are deposited on, forming platelets called splats. These splats build up many layers, resulting in a coating with a certain thickness. The application of tantalum carbide and zirconium cobalt alloy coatings on pistons is revolutionizing the automotive sector due to their remarkable durability and performance. These cutting-edge coatings, which are composed of ZrO_2 and TaC, have great advantages that extend the life and efficiency of pistons in internal combustion engines.^{3,4} Improving the resistance of pistons to wear, heat and corrosion is the main goal of coating them with ZrO_2 and TaC. These coatings have exceptional mechanical qualities, such as good temperature stability, low friction coefficient and high hardness.^{3,5} They can therefore tolerate the severe operating conditions found inside the engine, which include high temperatures, high pressures and continuous friction.^{4–7} Manufacturers can greatly increase the lifespan of pistons and lower the frequency of replacements and related maintenance expenses by using ZrO_2 and TaC coatings. Furthermore, by lowering the frictional losses and enhancing the heat dissipation, these coatings help to improve fuel efficiency.^{6,8} This results in decreased emissions, improved engine performance, and ultimately, a more ecologically friendly and sustainable driving experience. In recent times, there has been a substantial increase in the need for advanced materials exhibiting enhanced high-temperature characteristics. This surge in demand can be attributed to their pivotal role in diverse sectors including aerospace, energy and automotive.^{7–10} Materials used in high-temperature applications need the preservation of their inherent properties and structural integrity across a range of temperatures. The criticality of high-temperature stability cannot be overstated when considering materials that are exposed to exceedingly elevated thermal conditions.^{9,11} Thermal conductivity, an essential property, assumes a pivotal role in the processes of heat transfer and dissipation. The mechanical strength of materials holds significant importance, especially in high-temperature environments where maintaining structural integrity is crucial, alongside their thermal properties.^{10,12} Hence, the investigation of superior mechanical, thermal and thermomechanical properties is of great scientific significance. As the temperature rises, the physical and mechanical characteristics of materials experience alterations, resulting in a decline in material properties and diminished structural dependability.^{11,13} Sivakumar and Kumar conducted a study to investigate the effects of yttria stabilized zirconia coating on the performance of diesel engines and the pollutants they produce.^{12,14} A comparison

was made between the impact of the thermal barrier coating (TBC) on the performance and emission metrics and the characteristic curves of the baseline engine. The material's notable characteristics, such as its high thermal expansion coefficient, low thermal conductivity, high Poisson's ratio and stable phase structure at elevated temperatures, are easily noticeable.^{13–16} The experiment improved thermal efficiency by 5 %, decreased heat loss to the cooling medium by 5 %, decreased HC emission by 35 %, decreased brake specific fuel consumption by 28.3 % and raised thermal efficiency by 5 %. The aim of this research is to explore the impact of ZrO₂ and TaC coatings on a piston by altering their proportions. To the authors knowledge and from the literature above plenty of work has been carried on material performance coating on the piston to improve the efficiency like indicated power, fuel consumption, emission, *etc.*, but only few researchers are focused on the evaluating of the zirconium oxide and tantalum coating. This study seeks to demonstrate the influence of varying coating percentages on the surface morphology and quality of the component. This study will present the surface features, the microstructure as depicted in SEM images, and the mechanical attributes of the examined piston. The findings demonstrate that the active polar oxygen-containing functional groups are introduced onto the PET surface as a result of plasma modification.³⁴ The coating provides exceptional resistance to exposure to abrasive chemicals, mechanical strength against extensive abrasion, and high hardness for the substrate.³⁵

EXPERIMENTAL

Materials, methods and experimentation

The tantalum carbide nano-powder was purchased by US Research Nano materials Inc. The ZrO₂ was purchased Sigma Aldrich. The chemical composition is shown in Fig. 1a. The coating is performed on the aluminium alloy which is used as a substrate shown in Fig. 1b–d. The coating is done by plasma spray coating process, using varying process parameters on Spraymet Surface Technologies Pvt. Ltd., Bangalore. Fig. 1e shows the machine which consists of 3MB of plasma spray gun, nozzle with Group hole (GH) nozzle type, stand-off distance of maximum of 101 mm with the pressure of hydrogen of 3.5 bar and the flow rate up to 450 m/s. The samples were received and placed into a graphite crucible with a mixed powder composition of 95 % ZrO₂ + 5 % TaC, 98 % ZrO₂ + 2 % TaC and 100 % ZrO₂, then the coating was carried out on the samples using supersonic plasma spraying. The crucible was subsequently placed in a furnace and maintained at a temperature of 2000–2200 °C for a duration of 2 h. The TaC grains had a size ranging from 1–1.5 mm. The primary and carrier gas used was argon, while hydrogen served as the secondary gas. The samples were examined by the field emission scanning electron microscope (FESEM) FEI make, Quanta 200F model. The chemical composition of the coated piston, which had different compositions, were analysed using a FEGSEM and an attached energy-dispersive X-ray (EDX) spectrometer, the magnification varied from 10×–300,000×, with a resolution of 5 nm. The X-ray diffraction (XRD) pattern of the ZrO₂ and TaC powder was obtained using a powder X-ray diffractometer done in SRM institute of Science and Technology, Chennai, having PAN analytical make with Benchtop Shimadzu model with CuKα radiation. The size of the crystallite was calculated by X-ray

spectrum peaks using Scherrer's formula. To validate the coating, the samples were subjected to surface morphology and porosity measurement using image analysis software with ASTMB487 standards (De-winter material plus version-2 wth a magnification 50 \times -800 \times with 5 megapixel camera at Metmech Analytical Engineers, Chennai).

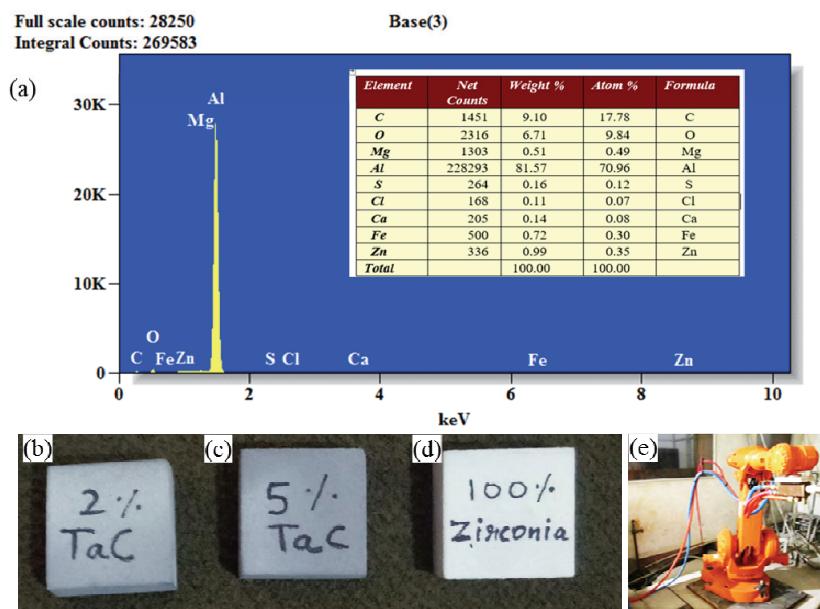


Fig. 1. a) Chemical composition of aluminum alloy, b) 98 % + 2 % TaC, c) 95 % ZrO₂ + 5 % TaC, d) 100 % ZrO₂ and e) plasma spray machine (Spraymet Surface Technologies Pvt. Ltd.).

RESULTS AND DISCUSSION

Fig. 2 shows the TaC and ZrO₂ powder XRD pattern reveals that the presence of diffraction peaks in the pattern indicates a high degree of crystalline nature the diffraction angles. TaC powder shows standard cubic structure with 2θ values of 34.9260, 40.5480, 58.6870, 70.1470, 73.7650 and 87.7400°; TaC powder have pattern reflection of (*h k l*) of (0 2 0), (0 2 2), (1 3 1), (2 2 2) and (0 4 0) which satisfy the JCPDS 96-101-0655. Regarding the diffraction peaks of ZrO₂ shows monoclinic crystal system, they become more distinct and smaller, and their intensity noticeably increases. This indicates a significant improvement in the crystallinity of the ZrO₂ nanocrystals. The enhancement is due to the enlargement of particle size, which leads to an increase in the number of crystalline planes.

The EDS pattern signified the existence of Zr, O and C, without any contamination from impurities shown in Fig. 3a. In contrast, the interior layer, which has been partially oxidized, appears to be more compact and largely composed of ZrO₂ components. The micro-particle-like diameters of some ZrO₂ match XRD

results, indicating amorphous compounds, which agrees with the results.^{18–20} The SEM image shows in Fig. 3b the aggregation 100 nm of the average size having the appearance of the particles in the shape of micro crystal with non-homogeneous particles sphere with the interstitial spaces between the spheres.

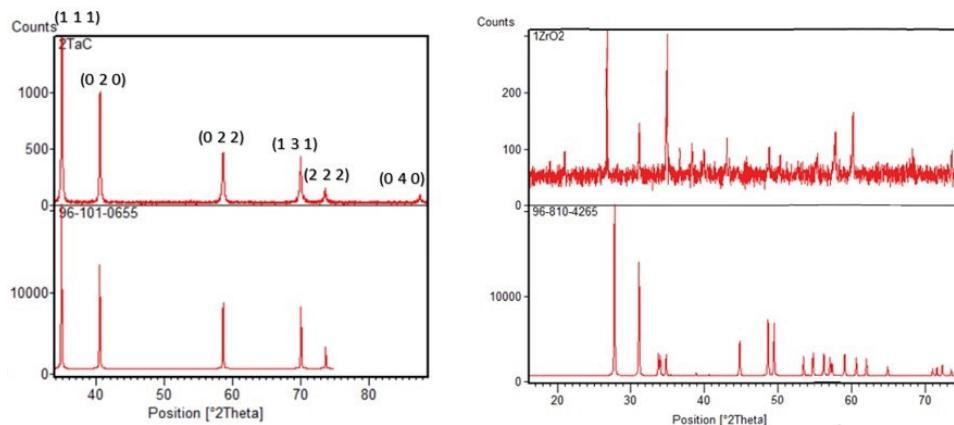


Fig. 2. XRD patterns for TaC and ZrO₂.

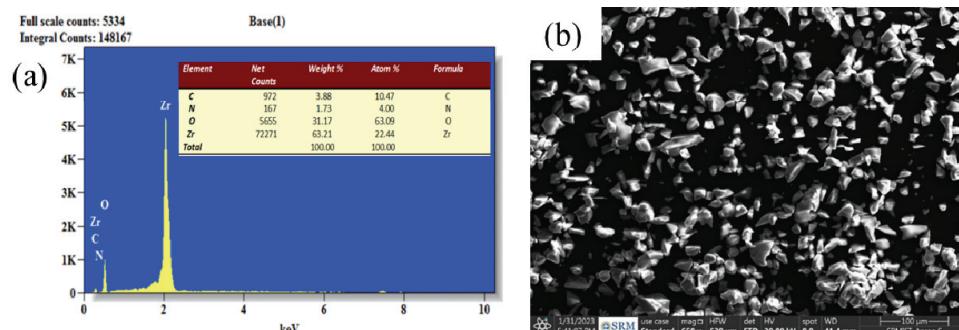


Fig. 3. a) EDS and b) powder SEM analysis for zirconium oxide.

Fig. 4a and b show the images acquired by SEM and EDX of tantalum powder which reveals the irregular or rise and fall surface.

Fig. 5a and b reveal that the ZrO₂ coating on aluminium alloy exhibits a granular structure which is densely packed with pores. The inadequate heat conduction between the ZrO₂ particles during the deposition phase results in partial melting.^{15,21} The amalgamation of partially and entirely liquefied ZrO₂ particles results in the formation of pores on the surface. When ZrO₂ is sprayed, it has a reaction with the gas molecules nearby, leading to a proper distribution of the coating on the substrate. The presence of oxide molecules in the air acts as a barrier, preventing the molten ZrO₂ particles from adhering to the substrate during

the deposition process.^{16,22} Moreover, the intense stress encountered during the solidification of ZrO₂ leads to the development of micro-cracks inside its structure. A layer of ZrO₂ has been applied to the surface of the aluminium alloy, resulting in a visible white zone. The spherical shape of the spray-dried composite powder is evident. The utilization of nanoscale particles as starting materials enables the fabrication of nanostructured powders that possess a homogeneous distribution of ZrO₂. The stability of the ceramic coatings is ensured by the plasma spraying process, which allows for optimal fluidity and homogeneous heating.^{17,23} The coatings exhibit predominantly tetragonal ZrO₂ phases, indicating the successful suppression of the change to the monoclinic phase.

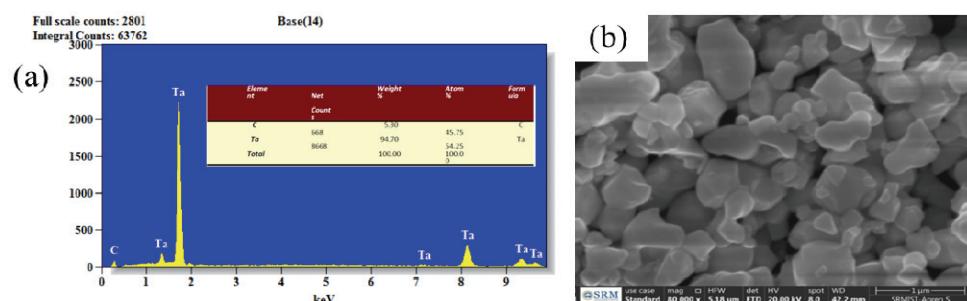


Fig. 4. a) EDS and b) powder SEM analysis for tantalum carbide.

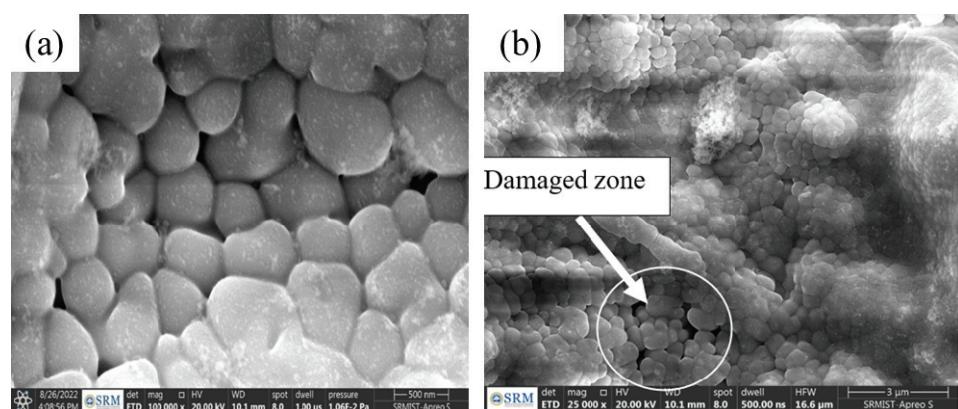


Fig. 5. a) 100 % ZrO₂ coated aluminium alloy; b) apparent gaps near the intersection (100 % ZrO₂ coated aluminium alloy).

The coating composed of 95 % ZrO₂ and 5 % TaC has a columnar structure and lacks sensitive regions such as grain boundaries, dislocations and second-phase precipitates. The columns have a width ranging from 30 to 60 μm. The structure of the coating exhibits quasi-regular vertical fissures that span the whole surface. The high-magnification photos reveal that the structural parts of

the coating primarily have a size ranging from 0.2 to 1 μm , which aligns with the size of the particles that collide with the surface of the substrate. The higher density of the SPS coating is linked to a larger average particle size of material clusters in the suspension, ranging from 1 to 5 μm . The absence of unmelted particles in the coating suggests that the plasma jet has generated enough thermal power. The coating often exhibits a size structure with splats ranging in thickness from 1 to 3 μm . The surface morphology changed from a common pancake-shaped structure to a cluster-shaped structure, depending on the concentrations of ZrO_2 and TaC . Similar observations were also reported.^{20,24}

Furthermore, the interface layer of the 95 % ZrO_2 and 5 % TaC coatings does not show significant defects or pores due to the stability of the process shown in Fig. 6a and b. Fig. 6c and d show the microstructure of the intersection area which shows minimum pores. The porosity measurement shows minimum pores area of 1.801 % and the non-porous area of 98.19 %, Fig. 6e. The TaC particles were unable to react with aluminium, compromising the interfacial bonding strength.

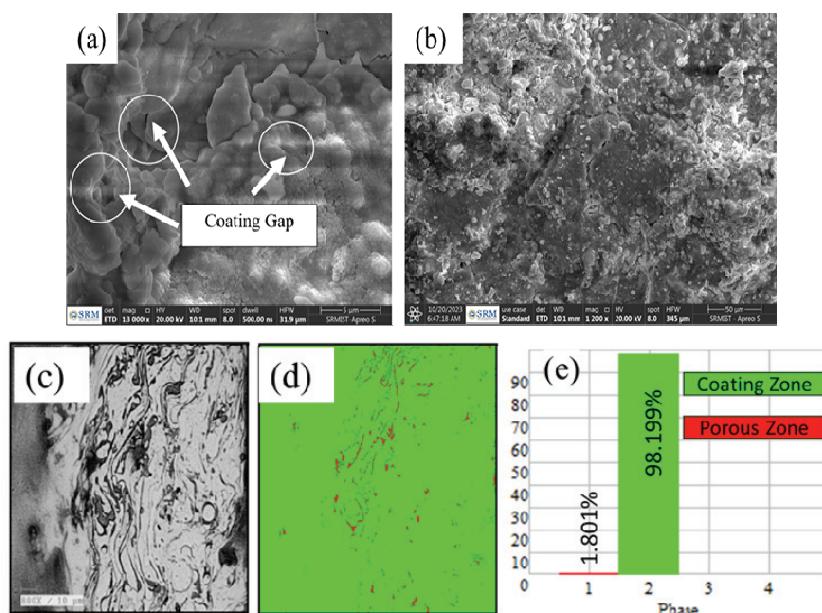


Fig. 6. a) Morphology of the coated surface; b) few pores on 95 % ZrO_2 + 5 % TaC coating surface; c) and d) microstructure and phase analysis; e) porosity measurement.

The plasma spraying method causes the described flaws when the surrounding gas interacts with the molten ZrO_2 droplets. Subsequently, when the droplets are deposited on the surface of the substrate, holes are formed due to inadequate overlap and quick solidification trapping internal gas.²⁷ The thickness of the

coatings, as determined by the cross-sectional analysis, increases simultaneously with ZrO_2 concentration. Beyond a concentration of 3 g/L of ZrO_2 , the inner layer suffered severe damage, leading to a halt in the increase of thickness. Nevertheless, up to this point, the trend of thickness increase becomes more prominent. This finding proves the ZrO_2 coating was adequately applied to the aluminium alloy. The presence of polyhedral or spherical grains, as well as unevenly formed grains, characterizes the densified microstructure. These granules are tightly bound together, providing a strong barrier that efficiently prevents oxygen from penetrating the piston material's surface.²⁹ Furthermore, the coating's structure contains a trace of mullite, which may be detected by its finest needle-shaped crystals. It should be noted that the powder rapidly melts and conducts a partial reaction with the oxygen present in the surrounding air during the spraying operation.

Microcracks, in other words the pores with dense structure, are seen in the plasma-sprayed ZrO_2 coating shown in Fig. 7a and b. In the examination carried out by EDX shown in Fig. 7c, Zr was identified in the luminous sections of the TaC layer within the ZrO_2 -TaC coating applied on the aluminium alloy. In reg-

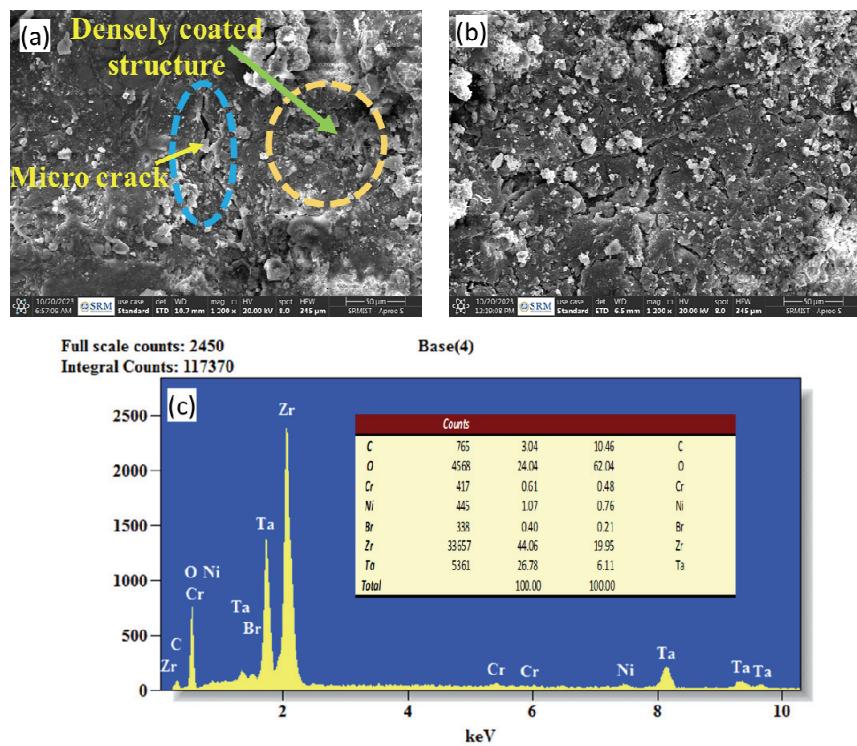


Fig. 7. a) 95 % ZrO_2 and 5 % TaC zone of dense particle, b) tiny pores on a coated surface (95 % ZrO_2 and 5 % TaC), c) EDX of the coated sample.

ard to the dynamic segregation theory for ZrO_2 , the reaction mechanism of ZrO_2 particles offers additional insight. It is theoretically possible for the reactive elements, even in their oxide form, to enhance the oxidation resistance.^{18,25} The participation of Zr in oxidation was observed in the study of ZrO_2 nanoparticles, ultimately being released from the ZrO_2 particles through reactions with Al.^{19,26} Furthermore, the interfaces between the coatings and substrates are transparent and strongly adhered, and the resulting coatings are homogeneous, dense, and of sufficient quality.

This provides more evidence that the process is unstable at higher concentrations, more especially the nano particles concentration of ZrO_2 which is around 8 g/L. Damage is caused to the inner layer or interface when larger concentrations are present, such as when there is 98 % ZrO_2 and 2 % TaC or when there is 100 % ZrO_2 .

The surface consisting of 98 % ZrO_2 and 2 % TaC was entirely coated with a cluster-like formation. The presence of ZrO_2 nanoparticles and localised plasma discharges contribute to the production of cluster-like formations. This phenomenon decreases the intensity of the discharges and causes instability.²⁸ With an increase in processing time, there is a corresponding increase in the size of the pancakes, which is a typical characteristic observed in plasma coating. Nevertheless, the impact of different ZrO_2 concentrations on this rise was not as prominent. Furthermore, the morphology of the pancakes was altered as the concentration of ZrO_2 increased, shifting from the uniform spherical shapes to the irregular and fragmented shapes shown in Fig. 8a. The reason for this could be attributed to the elevated content of ZrO_2 , which hampers the even dispersion of discharge channels. Regions that appear bright correspond to locations with a greater abundance of Zr, whereas the regions that appear dark correspond to areas with a lesser abundance of Zr. The presence of brilliant patches around the discharge channel is observed for low concentrations of ZrO_2 .²⁹ In addition, a multitude of minuscule pores appeared on the surface of the ZrO_2 coating. These pores can be linked to the chemical reaction between TaC and the gaseous by-products of SiO(g) , CO(g) and $\text{H}_2\text{(g)}$, Ni and N shown in Fig. 8b. Evidently, the interlayer cracks, resulting from thermal mismatch, originated in the ZrO_2 covering and separated the scale into two distinct sections. The damage occurs when a greater amount of ZrO_2 species is transported through the low-intensity discharge sparks, which do not induce interactions with the supplied species and thus harm the pre-existing inner layers. The porosity of this sample shows the maximum pore of 15.515 % with the coated area of 84.485 % shown in Fig. 8c and d, respectively. The aforementioned trend is less conspicuous in coatings including 95 % ZrO_2 with 5 % TaC, as well as those composed entirely of 100 % ZrO_2 , when compared to the coating consisting of 98 % ZrO_2 with 2 % TaC and its elements shown in Fig. 8e.

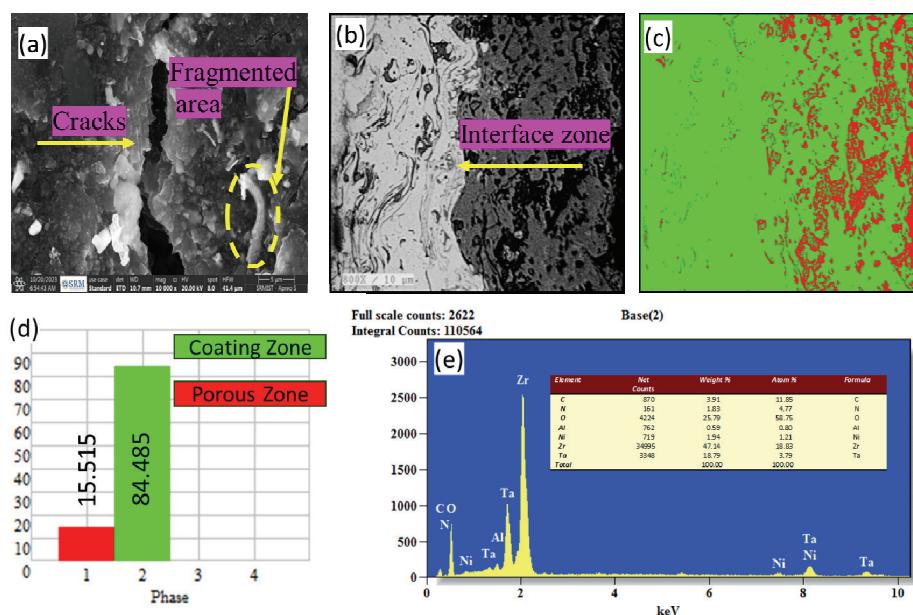


Fig. 8. a) 98 % ZrO_2 + 2 % TaC coating; b) and c) microstructure and phase analysis; d) porosity measurement; e) EDX analysis.

Following a thorough analysis, it was identified that the spray-applied coating possesses a compact microstructure.³⁰ This microstructure is made up of totally melted regions interspersed with a few particles that have remained unmelted. Surprisingly, a two-phase material is created within the coating when the temperature is elevated to 1400 °C.³¹ This substance is made up of cubic zirconia dioxide, which has a white appearance, and hexagonal corundum, which has a dark grey colour. Also, the coating possesses the occupied area of 84.485 % and the porosity of it includes 15.515 %. Thus, it may be inferred that an increased concentration of ZrO_2 and an extended processing duration can lead to severe damage to the inner layers which is consistent with earlier reports.^{32,33}

CONCLUSIONS

1. The microstructure of the zirconium dioxide and titanium aluminium carbide plays a crucial role in influencing the metallurgical and mechanical attributes of the surface coating. The oxide molecules in the air serve as a barrier, impeding the melted ZrO_2 particles from adhering to the substrate during deposition.
2. The appearance of the surface changed from a usual flat structure to a structure resembling clusters, with different amounts of ZrO_2 and TaC. Specifically, the surface with 98 % ZrO_2 and 2 % TaC was completely covered by the cluster-like structure.

3. Higher concentrations of ZrO_2 in the coatings lead to the increased interaction with discharge sparks and the instability of the process. The concentrations of 98 % ZrO_2 and 2 % TaC or 100 % ZrO_2 result in damage to the inner layer/interface. Higher concentrations and longer processing time can cause severe damage to the inner layers.

4. The plasma-sprayed ZrO_2 coatings exhibit microcracks and pores due to the interaction of gas with molten ZrO_2 droplets. The amount of thickness of the coatings is directly proportional to the concentration of ZrO_2 and the duration of the processing. The uneven layers and the particle fusion are observed in the ZrO_2 coating, while the ZrO_2 coating also has a relatively dense structure with cracks and tiny pores.

5. At elevated temperatures, a two-phase solid was made up of hexagonal corundum and cubic zirconia dioxide. It was made up of polyhedral or circular grains and a small amount of mullite.

Acknowledgement. The authors are very much thankful to St. Joseph's College of Engineering, OMR-Chennai.

ИЗВОД

ПОВЕЋАЊЕ ДУГОВЕЧНОСТИ И ПЕРФОРМАНСИ: ЕФЕКТИ ZrO_2 И ТАС ПРЕМАЗА НА КЛИПОВЕ У МОТОРИМА СА УНУТРАШЊИМ САГОРЕВАЊЕМ

SATHISH RENGARAJAN¹, RAMEEZA MUHAMMED¹, D. VIJAYAN² и MUHAMMED ABRAR³

¹Department of Mechanical Engineering, St. Joseph's College of Engineering OMR, Chennai, Tamil Nadu, India, ²Department of Mechanical Engineering, SCSVMV University, Enathur, Kanchipuram, Tamil Nadu, India и ³Department of Mechanical Engineering, St. Joseph's Institute of Technology, OMR, Chennai, Tamil Nadu, India

Облагање клипова са ZrO_2 и TaC побољшава њихову дуговечност и перформансе у моторима са унутрашњим сагоревањем повећавајући отпорност на хабање, топлоту и корозију. У овом истраживању вршило се наношење плазма спреја на круну клипа комбинацијом процентуалног састава и то 95 % ZrO_2 + 5 % TaC, 98 % ZrO_2 + 2 % TaC и 100 % ZrO_2 . Најбоље резултате показао је састав 95 % ZrO_2 + 5 % TaC. Повећање садржаја ZrO_2 доводи до формирања интегрисаније скале са мање пора. Веће концентрације ZrO_2 у премазима доводе до повећане интеракције са варницима приликом процеса пражњења и доводе до нестабилности процеса. На повишеним температурама настаје двофазни материјал од кубног цирконијум-диоксида и хексагоналног корунда. На снагу везивања премаза утиче додавање TaC, као и улазна снага током операције распршавања. Микроструктуру ZrO_2 и TaC превлака на легури алуминијума карактерише грануларна структура, чврсто збијене поре и делимично растопљене честице ZrO_2 . Превлака је имала уједначену структуру са стубастим и кластероликим елементима, под утицајем концентрације ZrO_2 .

(Примљено 24. јануара, ревидирано 8. априла, прихваћено 21. маја 2024)

REFERENCES

1. P.L. Fauchais, J.V.R. Heberlein, M.I. Boulos, *Overview of Thermal Spray*. In: *Thermal Spray Fundamentals*, Springer, Boston, MA, 2014, p. 17 (https://doi.org/10.1007/978-0-387-68991-3_2)
2. L. Pawlowski, *The Science and Engineering of Thermal Spray Coatings*, 2. ed., Wiley, New York, 2008 (ISBN 978-0-471-49049-4)
3. Y. Hu, Q. Dou, Q. Fu, X. Li, L. Zhou, J. Zhang, *Surf. Coat. Technol.* **435** (2022) 128243 (<https://doi.org/10.1016/j.surfcoat.2022.128243>)
4. Y. Zhang, J. Sun, L. Guo, X. Zhang, D. Cui, Q. Fu, *Corros. Sci.* **205** (2022) 110423 (<https://doi.org/10.1016/j.corsci.2022.110423>)
5. Z. Fu, X. Li, Y. Ren, M. Zhang, X. Geng, Q. Zhu, J.G. Li, X. Sun, *J. Eur. Ceram. Soc.* **39** (2019) 4996 (<https://doi.org/10.1016/j.jeurceramsoc.2019.07.011>)
6. Z. L. Mao, X. J. Yang, S. L. Zhu, Z. D. Cui, Z. Y. Li, Y. Q. Liang, *Mater. Express.* **5** (2015) 518 (<https://doi.org/10.1166/mex.2015.1267>)
7. G. Feng, H. Li, X. Yao, L. Chen, Y. Yu, H. Wang, M. Chen, *Ceram. Int.* **47** (2021) 21721 (<https://doi.org/10.1016/j.ceramint.2021.04.187>)
8. N. B. Dahotre, S. J. S. Nayak, *Surf. Coat. Technol.* **194** (2005) 58 (<https://doi.org/10.1016/j.surfcoat.2004.05.006>)
9. Z. Yao, Z. Song, H. Hao, Z. Yu, M. Cao, S. Zhang, M.T. Lanagan, H. Liu, *Adv. Mater.* **29** (2017) 1601727 (<https://doi.org/10.1002/adma.201601727>)
10. C. Suryanarayana, *Research* **10** (2019) 4219812 (<https://doi.org/10.34133/2019/4219812>)
11. V. Gvozdetskyi, B. Owens-Baird, S. Hong, and J.V. Zaikina, *Mater.* **12** (2018) 48 (<https://doi.org/10.3390/ma12010048>)
12. L. Wang, D. C. Li, J. S. Yang, F. Shao, X. H. Zhong, H. Y. Zhao, K. Yang, S. Y. Tao, Y. Wang, *J. Eur. Ceram. Soc.* **36** (2016) 1313 (<https://doi.org/10.1016/j.jeurceramsoc.2015.12.038>)
13. R. Darolia, *Int. Mater. Rev.* **58** (2013) 315 (<https://doi.org/10.1179/1743280413Y.0000000019>)
14. G. Sivakumar, S. S. Kumar, *Alex. Eng. J.* **53** (2014) 787 (<https://doi.org/10.1016/j.aej.2014.08.003>)
15. E. Vural, S. Ozel, B. Ozdalyan, *Optoelectr. Adv. Mat.* **8** (2014) 515 (<https://oamrc.inoe.ro/articles/the-investigation-of-microstructure-and-mechanical-properties-of-oxide-powders-coated-on-engine-pistons-surface/fulltext>)
16. J. Liang, Z. Peng, R. Li, B. Wang, *Ceram. Int.* **49** (2023) 29133 (<https://doi.org/10.1016/j.ceramint.2023.06.192>)
17. L. K. Brar, G. Singla, O. P. Pandey, *RSC. Adv.* **5** (2015) 1406 (<https://doi.org/10.1039/C4RA12105H>)
18. R. Sukanya, S. Ramki, S. M. Chen, *Microchim. Acta* **187** (2020) 342 (<https://doi.org/10.1007/s00604-020-04314-7>)
19. D. Manoharan, A. Loganathan, V. Kurapati, V. J. Nesamony, *Ultrason. Sonochem.* **23** (2015) 174 (<https://doi.org/10.1016/j.ultsonch.2014.10.004>)
20. E. A. Abdel Wahab, K.S. Shaaban, R. Elsaman, E. S. Yousef, *Appl. Phys., A* **125** (2019) 869 (<https://doi.org/10.1007/s00339-019-3166-8>)
21. M. Kovaleva, I. Goncharov, V. Novikov, M. Yapryntsev, O. Vagina, V. Sirota, Y. Tyurin, O. Kolisnichenko, *Mater. Today: Proc.* **49** (2022) 1423 (<https://doi.org/10.1016/j.matpr.2021.07.132>)

22. I. Gulyaev, V. Kuzmin, E. Kornienko, S. Vashchenko, D. Sergachev, *Mater. Today: Proc.* **11** (2019) 430 (<https://doi.org/10.1016/j.matpr.2019.01.008>)
23. Z. U. Rehman, D. Choi, *J. Magnes. Alloys* **7** (2019) 555 (<https://doi.org/10.1016/j.jma.2019.10.001>)
24. J. Jakubowicz, M. Sopata, G. Adamek, P. Siwak, T. Kachlicki, *Adv. Mater. Sci. Eng.* **2018** (2018) 2085368 (<https://doi.org/10.1155/2018/2085368>)
25. B. A. Pint, *Oxid. Met.* **45** (1996) 1 (<https://doi.org/10.1007/BF01046818>)
26. X. Luo, X. Yang, Q. Huang, A. Shi, C. Fang, Y. Weng, *J. Therm. Spray Technol.* **30** (2021) 1582 (<https://doi.org/10.1007/s11666-021-01215-w>)
27. G. Shao, Q. Wang, X. Wu, C. Jiao, S. Cui, Y. Kong, J. Jiao, X. Shen, *Corros. Sci.* **126** (2017) 78 (<https://doi.org/10.1016/j.corsci.2017.06.017>)
28. Y. H. Cui, Z. C. Hu, Y. D. Ma, Y. Yang, C. C. Zhao, Y. T. Ran, P. Y. Gao, L. Wang, Y. C. Dong, D. R. Yan, *Surf. Coat. Technol.* **363** (2019) 112 (<https://doi.org/10.1016/j.surfcoat.2019.02.059>)
29. G. Shao, X. Wu, S. Cui, X. Shen, Y. Lu, Q. Zhang, Y. Kong, *J. Alloys Compd.* **690** (2017) 63 (<https://doi.org/10.1016/j.jallcom.2016.08.073>)
30. A. A. Ali, S. A. Shama, A. S. Amin, S. R. EL-Sayed, *Mater. Sci. Eng., B* **269** (2021) 115167 (<https://doi.org/10.1016/j.mseb.2021.115167>)
31. R. Vaßen, D.E. Mack, M. Tandler, Y. J. Sohn, D. Sebold, O. Guillon, *J. Am. Cer. Soc.* **104** (2021) 463 (<https://doi.org/10.1111/jace.17452>)
32. D. Wang, B. Yang, Z. Tian, L. Shen, Y. Huang, *Trans. China Weld.* **34** (2013) 10 (<http://hjxb.hwi.com.cn/hjxb/en/article/id/20130303>)
33. K. H. Kim, S. Hoon, J. H. Kim, K. W. Hong, J. Y. Park, *J. Nanosci. Nanotechnol.* **17** (2017) 8598 (<https://doi.org/10.1166/jnn.2017.15171>)
34. S. Samipour, H. Taghvaei, D. Mohebbi-Kalhor, M. R. Rahimpour, *Surf. Innov.* **8** (2019) 76 (<https://doi.org/10.1680/jsuin.19.00030>)
35. K. Zhang, Y. Zhu, Z. Chen, Z. Zhang, Y. Gao, *Surf. Innov.* **40** (2022) 1 (<https://doi.org/10.1680/jsuin.22.01049>).