

SUPPLEMENTARY MATERIAL TO  
**Wet process of phosphoric acid purification by solvent  
extraction using tri-*n*-butyl phosphate and cyclohexanol  
mixtures**

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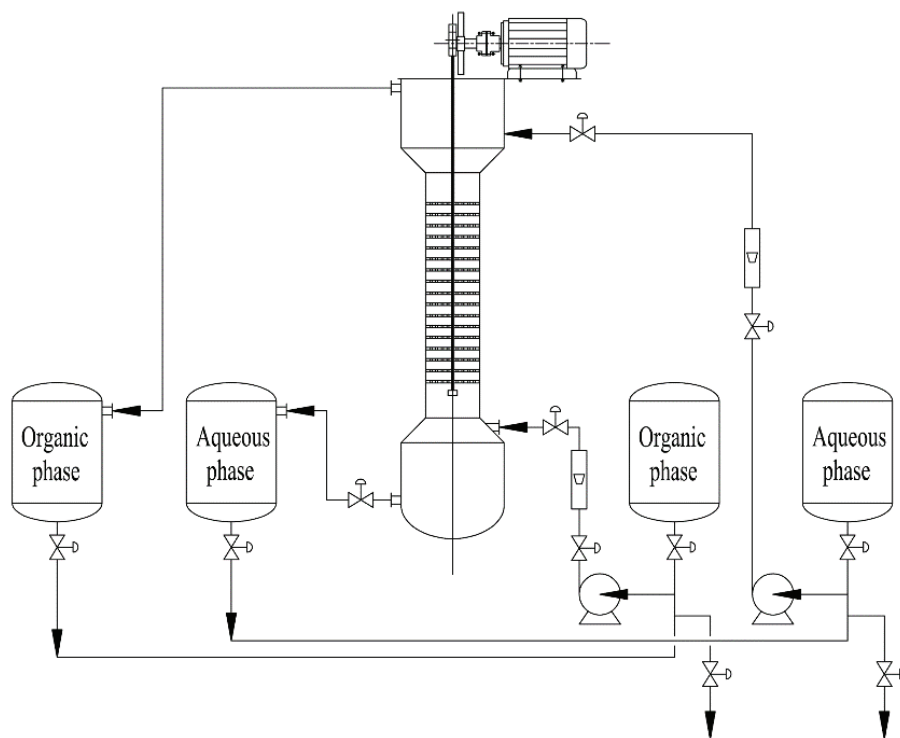


Fig. S-1. Schematic flow diagram of the reciprocating plate extraction column.

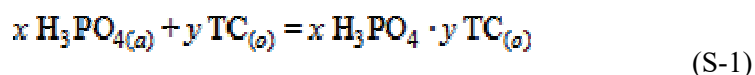
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TABLE S-I. Equilibrium data of the extraction system  $\text{H}_3\text{PO}_4$  (1)– $\text{H}_2\text{O}$  (2)–TC (34 % TBP + 66 % cyclohexanol) (3) at 298.2K and atmospheric pressure;  $w$  is the mass fraction (mass %); blanks: do not exist or not detected

Initial mixture			Aqueous phase			Organic phase		
$w_1$	$w_2$	$w_3$	$w_1$	$w_2$	$w_3$	$w_1$	$w_2$	$w_3$
51.00	16.00	33.00	69.53	25.49	4.98	48.70	11.97	39.33
48.00	18.00	34.00	64.72	30.78	4.50	41.98	11.92	46.10
40.00	23.00	37.00	55.75	40.41	3.85	31.25	11.62	57.13
33.00	27.00	40.00	48.52	48.46	3.02	22.40	10.55	67.05
26.00	31.00	43.00	41.22	55.84	2.94	17.07	9.78	73.15
18.00	36.00	46.00	35.89	61.40	2.71	14.37	9.20	76.44
11.00	39.00	50.00	26.47	70.52	3.01	7.00	8.89	84.11
8.28	41.72	50.00	15.49	81.26	3.25	2.22	8.42	89.36
	50.00	50.00		97.70	2.30		8.14	91.86

### Process stoichiometry

For the simplification of analysis method, the assumption is employed in which the binary solvent mixtures (34 % TBP + 66 % cyclohexanol) are treated as an entirety, TC. Then assuming that the  $\text{H}_3\text{PO}_4$  transfers from the aqueous phase into the organic phase in the form of  $\text{H}_3\text{PO}_4$  molecule and exists in the organic phase as a complex of the form  $x\text{H}_3\text{PO}_4 \cdot y\text{TC}$ <sup>1,2</sup>. The extraction reaction can be described as:



where  $x$  and  $y$  are the stoichiometric coefficients of  $\text{H}_3\text{PO}_4$  and TC in the reaction above, respectively. The subscripts a and o stand for the aqueous and organic phases, respectively.

The equilibrium constant ( $K_{\text{eq}}$ ) of the extraction reaction in Eq. (S-1) is:

$$K_{\text{eq}} = \frac{[x \text{H}_3\text{PO}_4 \cdot y \text{TC}]_{(o)}}{[\text{H}_3\text{PO}_4]_{(a)}^x \cdot [\text{TC}]_{(a)}^y} \quad (\text{S-2})$$

The distribution coefficient of  $\text{H}_3\text{PO}_4$  can be calculated as

$$D = \frac{[\text{H}_3\text{PO}_4]_{(o)}}{[\text{H}_3\text{PO}_4]_{(a)}} = \frac{x [x \text{H}_3\text{PO}_4 \cdot y \text{TC}]_{(o)}}{[\text{H}_3\text{PO}_4]_{(a)}} \quad (\text{S-3})$$

An indirect approximation method based on slope analysis was used to verify the stoichiometry of the extracted species. Inserting Eq. (S-3) into Eq. (S-2) and then taking the logarithm of both sides of the resulting equation leads to the expression:

$$\log D = \log x K_{\text{eq}} + (x-1) \log [\text{H}_3\text{PO}_4]_{(a)} + y \log [\text{TC}]_{(a)} \quad (\text{S-4})$$

Inserting Eq. (S-3) into Eq. (S-4) gives:

$$\log[\text{H}_3\text{PO}_4]_{(o)} = \log xK_{\text{eq}} + x\log[\text{H}_3\text{PO}_4]_{(a)} + y\log[\text{TC}]_{(o)} \quad (\text{S-5})$$

After determining the values of  $x$  and  $y$  in the extraction reaction in Eq. (S-1), the stoichiometry of the extracted complexes and the process can be obtained then.

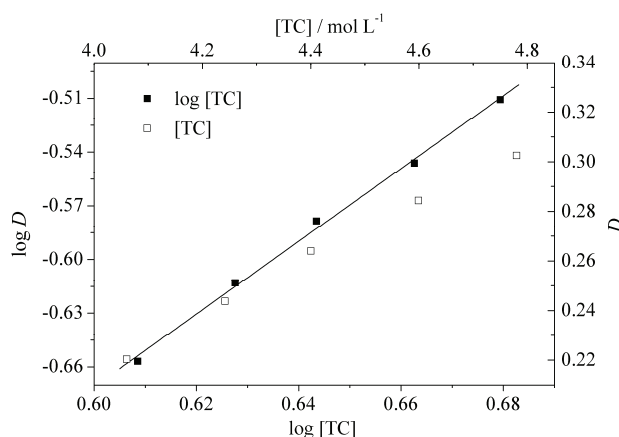


Fig. S-2. Effect of extractant concentration on the distribution coefficient of  $\text{H}_3\text{PO}_4$ :  $[\text{H}_3\text{PO}_4] = 9.16 \text{ mol L}^{-1}$ ,  $\text{O/A} = 4$ ,  $T = 298.2 \text{ K}$ ; (■)  $\log [\text{TC}]$ ; (□)  $[\text{TC}]$ .

A comparison of the IR spectrum of TC before (A) and after (B) extraction of  $\text{H}_3\text{PO}_4$  is shown in Figure S-3. The IR spectrum of TC shows a band at  $1024 \text{ cm}^{-1}$  which corresponds to the P–O–C bond stretching vibration of TBP. The peak at  $1024 \text{ cm}^{-1}$  broadens after extraction due to the superposition of the vibrations of P–O–C and P–O–H. The peak at  $1067 \text{ cm}^{-1}$  may be assigned to the stretching vibration of the C–O bond in cyclohexanol. Because of hydrogen bond formation after extraction, the electron cloud is distributed more averagely and the C–O bond stretching vibration frequency is lowered to  $1058 \text{ cm}^{-1}$ . A band at  $1272 \text{ cm}^{-1}$  is ascribed to the P=O bond stretching vibration of TBP. The peak at  $1272 \text{ cm}^{-1}$  shifted to lower frequency at  $1253 \text{ cm}^{-1}$ , which indicates that hydrogen bonds (P=O...H) formed between the oxygen atom of the phosphoryl group of the TBP molecule and the hydrogen atom of the  $\text{H}_3\text{PO}_4$  molecule. Another obvious difference between the spectra of TC before and after extraction is the appearance of bands at  $1647 \text{ cm}^{-1}$ , which represents O–H bond deformation vibrations. This is because certain amounts of –OH bonds for  $\text{H}_2\text{O}$  were extracted into the organic phase after extraction. The variation is mainly attributed to the partial solubility of water in the extractant, which is in agreement with the result of phase equilibrium study of the system  $\text{H}_3\text{PO}_4\text{--H}_2\text{O--TC}$ . Moreover, the –OH bond stretching vibration at  $3380 \text{ cm}^{-1}$  in cyclohexanol is shifted to a higher

frequency at  $3395\text{ cm}^{-1}$  and the peak widened. Based on these changes, it is concluded that  $\text{H}_3\text{PO}_4$  was extracted into the organic phase as well as  $\text{H}_2\text{O}$  molecules after extraction.<sup>2,3</sup> However, the structures of the extracted complexes and the formation process have not been determined. Further efforts are needed to clarify these issues.

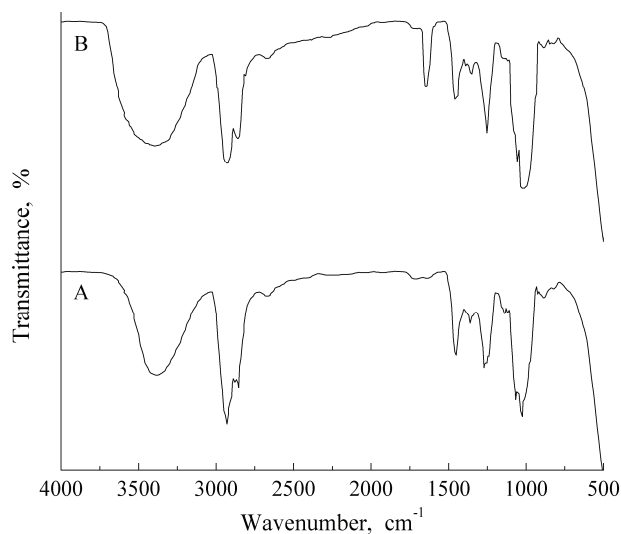


Fig. S-3. IR spectrum of TC before (A) and after (B) extraction.

#### *Effect of temperature on the extraction of $\text{H}_3\text{PO}_4$ and impurities*

According to the Van't Hoff equation:<sup>4</sup>

$$\frac{\Delta \log D}{\Delta(1/T)} = -\frac{\Delta H}{2.303R} \quad (\text{S-6})$$

plots of  $\log D$  versus  $T^{-1}$  are shown in Figs. S-4 and S-5. Then the values of the enthalpy change of extraction for  $\text{H}_3\text{PO}_4$  and impurities can be calculated. Using regression analysis, the following relations can be established from the obtained data:

For  $\text{H}_3\text{PO}_4$  extraction:

$$\log D = -1.35 + 0.22 \times (T^{-1}/10^{-3}), r = 0.999 \quad (\text{S-7})$$

For  $\text{Fe}^{3+}$  extraction:

$$\log D = -0.89 - 0.29 \times (T^{-1}/10^{-3}), r = 0.998 \quad (\text{S-8})$$

For  $\text{Mg}^{2+}$  extraction:

$$\log D = 2.14 - 1.28 \times (T^{-1}/10^{-3}), r = 0.999 \quad (\text{S-9})$$

For Al<sup>3+</sup> extraction:

$$\log D = 1.88 - 1.17 \times (T^{-1} / 10^{-3}), r = 0.999 \quad (\text{S-10})$$

For F<sup>-</sup> extraction:

$$\log D = 1.43 - 0.98 \times (T^{-1} / 10^{-3}), r = 0.997 \quad (\text{S-11})$$

For SO<sub>4</sub><sup>2-</sup> extraction:

$$\log D = -0.05 - 0.39 \times (T^{-1} / 10^{-3}), r = 0.999 \quad (\text{S-12})$$

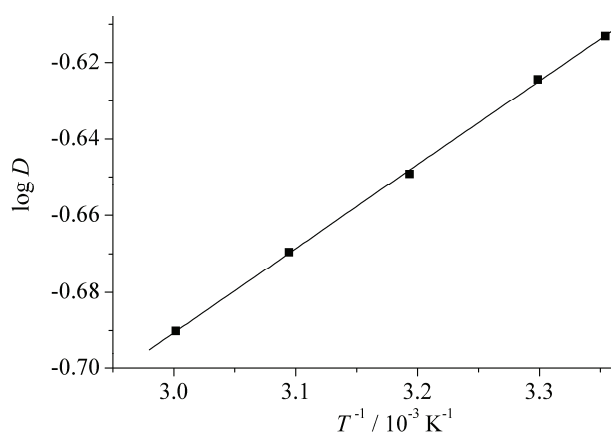


Fig. S-4. Effect of temperature on distribution coefficients of H<sub>3</sub>PO<sub>4</sub>: [TC] = 4.24 mol L<sup>-1</sup>, [H<sub>3</sub>PO<sub>4</sub>] = 9.16 mol L<sup>-1</sup>, O/A = 4.

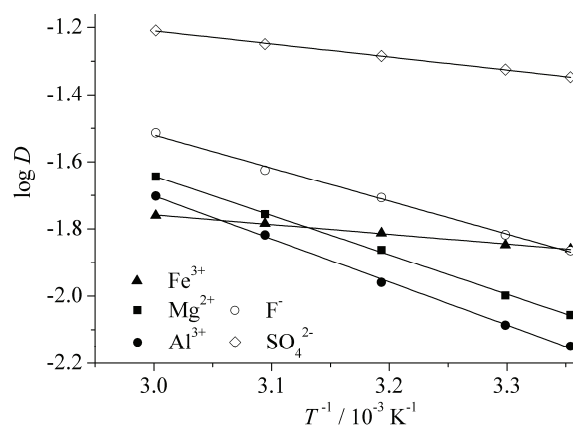


Fig. S-5. Effect of temperature on distribution coefficients of Fe<sup>3+</sup>, Mg<sup>2+</sup>, Al<sup>3+</sup>, F<sup>-</sup> and SO<sub>4</sub><sup>2-</sup>: [TC] = 4.24 mol L<sup>-1</sup>, [H<sub>3</sub>PO<sub>4</sub>] = 9.16 mol L<sup>-1</sup>, O/A = 4; (▲) Fe<sup>3+</sup>; (●) Mg<sup>2+</sup>; (■) Al<sup>3+</sup>; (○) F<sup>-</sup>; (◇) SO<sub>4</sub><sup>2-</sup>.

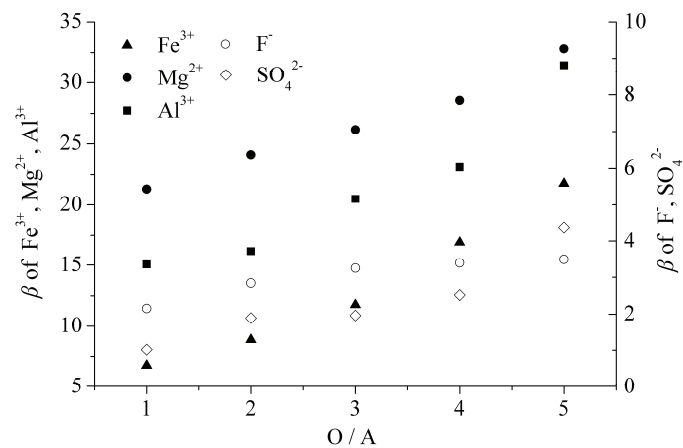


Fig. S-6. Effect of phase ratio on the separation factor for  $\text{Fe}^{3+}$ ,  $\text{Mg}^{2+}$ ,  $\text{Al}^{3+}$ ,  $\text{F}^-$  and  $\text{SO}_4^{2-}$ :  
 $[\text{TC}] = 4.24 \text{ mol L}^{-1}$ ,  $[\text{H}_3\text{PO}_4] = 9.16 \text{ mol L}^{-1}$ ,  $T = 298.2 \text{ K}$ ; (▲)  $\text{Fe}^{3+}$ ; (●)  $\text{Mg}^{2+}$ ;  
 (■)  $\text{Al}^{3+}$ ; (○)  $\text{F}^-$ ; (◇)  $\text{SO}_4^{2-}$ .

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